## THE PROPAGATION OF COMPRESSIVE-SHEAR PERTURBATIONS IN A NONLINEARLY ELASTIC MEDIUM

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1. Consider a homogeneous medium at rest occupying the lower half-space in Fig.1. We introduce a rectangular system of Lagrangean coordinates  $\partial xyz$ and consider the stress and small-strain tensors

$X_x$	Xy	Xz	$\epsilon_{xx}$	$\frac{1}{2} \epsilon_{xy}$	<sup>1</sup> /2 8 <sub>xz</sub>
$Y_x$	Yy	Y <sub>z</sub>	1/2 E <sub>xy</sub>	$e_{yy}$	<sup>1</sup> /2 ε <sub>yz</sub>
Xz	Yz	Zz	1/2 8 <sub>xz</sub>	$^{1}/_{2} \epsilon_{yz}$	ε <sub>zz</sub>

with first invariants

$$P = \frac{1}{3} (X_x + Y_y + Z_z), \qquad \varepsilon = \varepsilon_{xx} + \varepsilon_{yy} + \varepsilon_{zz}$$

and second invariants

$$T = \frac{1}{2}\sqrt{2}\sqrt{2}\sqrt{(X_x - Y_y)^2 + (Y_y - Z_z)^2 + (Z_z - X_x)^2 + 6(X_y^2 + X_z^2 + Y_z^2)}$$
  
$$F = \frac{1}{2}\sqrt{2}\sqrt{(\varepsilon_{xx} - \varepsilon_{yy})^2 + (\varepsilon_{yy} - \varepsilon_{zz})^2 + (\varepsilon_{zz} - \varepsilon_{xx})^2 + \frac{3}{2}(\varepsilon_{xy}^2 + \varepsilon_{xz} + \varepsilon_{yz}^2)}$$

respectively.

Suppose that the medium in question can be described by a model of a nonlinearly elastic body with the properties

$$P = \varphi(\varepsilon),$$
  $D_{\sigma} = 6QD_{\varepsilon},$   $T = f(\Gamma),$   $Q(\Gamma) \equiv \frac{f(\Gamma)}{6\Gamma}$ 

In these formulas  $D_{\sigma}$  and  $D_{\epsilon}$  are the stress and strain deviators  $\phi(\epsilon)$  and  $f(\Gamma)$  are known functions.

Suppose that at the initial moment of time t = 0 all particles lying on the surface of the medium (x = 0) are given one and the same velocity  $V_0(V_{x0}, V_{y0}, 0)$ , which then remains constant (Fig.1), where  $V_{y0} \ge 0$ . Plane uniform motion takes place within the medium, so that all parameters of motion depend only on x and t. We introduce a particle-velocity vector  $V(V_x, V_y, 0)$  and a particle-displacement vector U(u, v, 0). By virtue of symmetry of the problem, we have



Since  $V_x = \partial u / \partial t$  and  $V_y = \partial v / \partial t$ , we obtain from (1.1) that

$$\frac{\partial V_x}{\partial x} = \frac{\partial e}{\partial t}, \qquad \frac{\partial V_y}{\partial x} = \frac{\partial e_{xy}}{\partial t}$$
(1.4)

The equations of motion are of the form [1]

$$\rho_0 \frac{\partial V_x}{\partial t} = \frac{\partial X_x}{\partial x}, \qquad \rho_0 \frac{\partial V_y}{\partial t} = \frac{\partial X_y}{\partial x}$$
(1.5)

where  $\rho_0$  is the density of the medium at rest. Equations (1.2) to (1.5) form a closed system which must be solved for the conditions

$$V_x = V_{x0}, \quad V_y = V_{y0} \quad \text{for } x = 0,$$
 (1.6)

$$V_x = 0, V_y = 0, \quad \boldsymbol{\varepsilon} = 0, \quad \boldsymbol{\varepsilon}_{xy} = 0 \quad \text{for } x = \infty$$
 (1.7)

Making use of (1.3) and eliminating  $\chi_x$  and  $\gamma_y$  from (1.5), we obtain

$$\frac{\partial V_x}{\partial t} - a \frac{\partial e}{\partial x} - b \frac{\partial e_{xy}}{\partial x} = 0, \qquad \frac{\partial V_y}{\partial t} - b \frac{\partial e}{\partial x} - c \frac{\partial e_{xy}}{\partial x} = 0$$
(1.8)

Here

$$a = \frac{1}{\rho_0} \left( \frac{d\varphi}{dE} + 4Q \left( \Gamma \right) + \frac{4\epsilon^2}{\Gamma} \frac{dQ}{d\Gamma} \right), \qquad b = \frac{1}{\rho_0} \frac{3\epsilon\epsilon_{xy}}{\Gamma} \frac{dQ}{d\Gamma}$$
$$c = \frac{1}{\rho_0} \left( 3Q \left( \Gamma \right) + \frac{9}{4} \frac{\epsilon_{xy}^2}{\Gamma} \frac{dQ}{d\Gamma} \right)$$
(1.9)

It can easily be seen that the characteristics of the system (1.4), (1.8) may be found from Equation

$$dx / dt)^2 = \frac{1}{2} \left[ a + c \pm \sqrt{(a - c)^2 + 4b^2} \right]$$

For the existence of four families of characteristics we have the condition  $a + c > V(\overline{a-c})^3 + 4b^3$ , or

$$\left(Q + \frac{3\boldsymbol{e}_{xy}^{2}Q'}{4\Gamma}\right)\varphi' + 4Q\left(Q + Q'\right) > 0$$
(1.10)

Since  $\varphi(\varepsilon)$  and  $Q(\Gamma)$  are in essence independent functions, it follows that the inequality  $Q + \Gamma Q' > 0$  is necessary if (1.10) is to nold. It can be shown that it would also be a sufficient condition for (1.10), if  $\varphi' > 0$ (which is natural). We make the assumption that the inequality  $Q + \Gamma Q' > 0$ always holds. It is easily seen that a necessary and sufficient condition for this inequality to hold is that the function  $T(\Gamma)$  increases monotonically.

With these assumptions the system has four families of characteristics

$$\left(\frac{dx}{dt}\right)_{1}^{2} = \pm \frac{a+c+\sqrt{(a-c)^{2}+4b^{2}}}{2}, \qquad \left(\frac{dx}{dt}\right)_{2}^{2} = \pm \frac{a+c-\sqrt{(a-c)^{2}+4b^{2}}}{2} \tag{1.11}$$

It will be noted that in the case of pure compression (or expansion) without shear ( $V_{y} = 0$ ,  $\epsilon_{x,y} = 0$ ) the system (1.4), (1.8) has two families of characteristics given by the formula for  $(dx/dt)_{1}$ . In case of pure shear  $(V_{\tau}\equiv 0,\,\epsilon\equiv 0)$  this system has two families of characteristics given by the formula for  $(dx/at)_2$ .

For this reason we shall call the characteristics  $(dx/dt)_1$  and  $(dx/dt)_2$  compression and shear characteristics, respectively. It can easily be shown that

$$\left|\left(\frac{dx}{dt}\right)_{1}\right|^{2} > \left|\left(\frac{dx}{dt}\right)_{2}\right|^{2}$$

2. In view of the self-similarity of the problem under discussion we conclude that the parameters  $V_x$ ,  $V_y$ , e.  $e_{xy}$ ,  $X_x$  and  $X_y$  depend only on the variable  $\xi = x/t$ . In this case the system (1.4), (1.8) is easily reduced to the form

$$\frac{dV_x}{d\xi} + \xi \frac{de}{d\xi} = 0, \qquad \frac{dV_y}{d\xi} + \xi \frac{de_{xy}}{d\xi} = 0$$

$$(\xi^2 - a) \frac{de}{d\xi} = b \frac{de_{xy}}{d\xi}, \qquad (\xi^2 - c) \frac{de_{xy}}{d\xi} = b \frac{de}{d\xi}$$

$$(2.1)$$

Conditions (1.6) and (1.7) become

 $V_{x} = V_{x0}, \qquad V_{y} = V_{y0} \quad \text{for } \xi = 0$   $V_{x} = 0, \qquad V_{y} = 0, \quad \varepsilon = 0, \quad \varepsilon_{xy} = 0 \quad \text{for } \xi = \infty$  (2.2)

The motion in a pure-compression (or expansion) wave adjacent to the zone at rest is described by equations obtained from (2.1) with  $V_y \equiv 0$ ,  $\epsilon_{xy} \equiv 0$ 

$$\frac{dV_x}{d\xi} + \xi \frac{d\varepsilon}{d\xi} = 0, \quad (\xi^2 - a_0) \frac{d\varepsilon}{d\xi} = 0 \qquad \left(a_0 = a_0(\varepsilon) = \frac{1}{\rho_0} \left[\varphi' + 4Q(|\varepsilon|)Q'(|\varepsilon|)\right]\right)$$
(2.3)

The general solution to the system (2.3) defines a constant flow

 $V_r = V_{r1} = \text{const}, \qquad \varepsilon = \varepsilon_1 = \text{const}$ 

the zone of which is separated from the zone at rest by a compression (or expansion) shock-wave. Taking into account (1.3), we can write the conditions on the shock-wave [1] in the form

$$V_{x1} + D\varepsilon_1 = 0, \qquad \rho_0 DV_{x1} = (X_{x1} - X_{x0})$$
  

$$X_{x0} = \varphi(0), \qquad X_{x1} = \varphi(\varepsilon_1) + 4Q(|\varepsilon_1|)\varepsilon_1 \qquad (2.4)$$

Here D is the (constant) velocity of the shock-wave, the parameters in the zone of constant flow behind the shock-wave being denoted by the suffix 1 The particular solution to the system (2.3) (a centered wave) is

$$\xi = \sqrt[4]{a_0} (\varepsilon), \qquad V_x = -\int_0^z \sqrt[4]{a_0} (\varepsilon) d\varepsilon$$

If for compressive (or tensile) deformations  $da_0/d|\varepsilon| < 0$ , then a centered compression (or expansion) wave will propagate through the undisturbed medium. If however  $da_0/d|\varepsilon| > 0$ , a compression (or expansion) shock-wave will travel in front. If  $a_0 \equiv \text{const}$ , a compression (or expansion) shock-wave travels in front also. For simplicity we shall not consider cases when  $da_0/d|\varepsilon|$  changes sign.

Consider now a chear-compression (or expansion) wave propagating through a region of pure compression (or expansion). The general solution to the system (2.1) defines the constant flow

$$V_x = V_{x2} = \text{const}, \quad V_y = V_{y2} = \text{const}, \quad \varepsilon = \varepsilon_2 = \text{const}, \quad \varepsilon_{xy} = \varepsilon_{xy2} = \text{const}$$

The region of constant flow accompanied by shear can be separated by a shock-wave from the region  $e_{xy} = 0$ ,  $V_y = 0$ . We can write down the conditions

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on this shock-wave, denoting the parameters in front of and behind the wave, respectively, by the suffixes 1 and 2  $(V_{x2} = V_{x0}, V_{y2} = V_{y0})$ . Suppose that the wave velocity relative to fixed space is b and the equation of the wave is

$$c = x^* = Ct$$

Then from the relations

$$\int_{0} bdt = x^{*} + u_{1}(x^{*}, t), \quad \varepsilon = \frac{\rho_{0}}{\rho} - 1, \quad u_{2}(x^{*}, t) = u_{1}(x^{*}, t), \quad v_{2}(x^{*}, t) = 0$$

we can easily obtain

$$(b - V_{x1}) \rho_1 = \rho_0 C, \quad V_{y0} = -C \epsilon_{xy2}, \quad V_{x0} = C \epsilon_2 = V_{x1} + C \epsilon_1 \quad (2.5)$$

and the relations [1]

$$\rho_1(b - V_{x1}) \ V_{y0} = -X_{y2}, \ \rho_1(b - V_{x1})(V_{x0} - V_{x1}) = -(X_{x1} - X_{x2})$$

assume the form

$$\rho_0 C V_{y_0} = -X_{y_2}, \quad \rho_0 C \left( V_{x_0} - V_{x_1} \right) = - \left( X_{x_1} - X_{x_2} \right) \tag{2.6}$$

Conditions (2.5) and (2.6) must be supplemented by Equations (1.3)

$$X_{x2} = C(\varepsilon_2) + 4\varepsilon_2 Q(\Gamma_2), \qquad X_{y2} = 3\varepsilon_{xy2} Q(\Gamma_2), \quad \Gamma_2 = \sqrt{\varepsilon_2^2 + 3/4 \varepsilon_2 \varepsilon_{xy2}} \quad (2.7)$$

For the shear-compression (expansion) shock-wave to be stable it is essential [2] for its velocity to be not less than the velocity of small shear perturbations ahead of the wave and not greater than the velocity of small shear and compression perturbations behind the wave. Simple computations show that the shock-wave will be stable if the inequality

$$Q'(\Gamma_2) \ge 0 \tag{2.8}$$

holds.

Consider now the particular solution of the system (2.1). Multiplying together the last two of Equations (2.1) and cancelling the product  $(de/d\xi)$   $(de_{xy}/d\xi)$ , assumed to be no-zero, we obtain  $(\xi^2 - a)(\xi^2 - c) = b^2$ .

From this we have that either

$$\xi = \left[\frac{1}{2}\left(a + c + \sqrt{(a - c)^2 + 4b^2}\right)\right]^{\frac{1}{2}}$$
(2.9)

or

$$\xi = \left[\frac{1}{2} \left(a + c - \sqrt{(a - c)^2 + 4b^2}\right)\right]^{\frac{1}{2}}$$
(2.10)

It can easily be shown that (2.9) cannot provide a solution to the problem. Indeed, a comparison of (2.9) and (1.11) shows that for the advancing

compression characteristics  $dx/dt = 5 = x/t_{p}$ i.e. in the zone of solution (2.9) the characteristics (2.9) are (in the xt-plane) rays emanating from the origin of coordinates. Consequently, the ray separating the regions of pure compression and shear-compression in the xt-plane is a compression characteristic. But this means that the front of the shearcompression shock-wave leaves behind the waves of small shear perturbations originating from the surface of the medium, since

$$\left(\frac{dx}{dt}\right)_1 \left| > \left| \left(\frac{\partial x}{\partial t}\right)_2 \right| \right|$$

This is not possible.

Consequently the particular solution is given by Formula (2.10) together with the first three of equations (2.1). The same



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Fig. 2

particular solution (2.9) corresponds to a leading pure compression wave. By analogous reasoning we conclude that in the zone of the particular solution the shear characteristics are rectilinear rays in the xt-plane. For this reason this solution is called a centered shear-wave. Ahead of the centered shear-wave there must be a region of constant flow, since the proximity of centered compression and shear waves requires the shear and compression characteristics to coincide on their boundary, which is not possible.

3. It follows from the above that the form of the solution depends on the form of the functions  $a_0(\epsilon)$  and  $Q(\Gamma)$ . If we do not consider the cases when  $a_0 = \text{const}$ ,  $Q \equiv \text{const}$  in view of their simplicity, then in all there can be four variants of the ensuing motion. We shall now consider these, assuming, in order to be specific, that  $V_{xo} > 0$  (compression):

 $da_{0}/d|\varepsilon| > 0,$   $dQ/d\Gamma > 0$ 

A pure compression shock-wave propagates throughout the undisturbed medium; behind this wave there is a zone of constant flow, through which a compression-shear shock-wave travels [7 and 8]. Between the second shock wave and the surface of the medium there is a zone of constant flow. The motion pattern in the xt-plane is shown in Fig.2.

The solution is of the form

$$\begin{aligned} \varepsilon &= 0, \quad \varepsilon_{xy} = 0, \quad V_x = 0, \quad V_y = 0, \quad \text{for } x > Dt \\ \varepsilon &= \varepsilon_1, \quad \varepsilon_{xy} = 0, \quad V_x = V_{x1}, \quad V_y = 0, \quad \text{for } Dt > x > Ct \\ \varepsilon &= \varepsilon_2, \quad \varepsilon_{xy} = \varepsilon_{xy2}, \quad V_x = V_{x0}, \quad V_y = V_{y0} \quad \text{for } Ct > x \ge 0 \end{aligned}$$
(3.1)

Here  $V_{\chi_1^0}$  and  $V_{y_1^0}$  are known quantities. In order to determine the constants  $\varepsilon_1$ ,  $\varepsilon_2$ ,  $\varepsilon_{\chi y_2}$ ,  $V_{\chi_1}$ , D, and C we have the system of equations (2.4) to (2.7). The above solution may be used for the experimental determination of the functions  $\varphi(\varepsilon)$  and  $Q(\Gamma)$ . From (2.4) to (2.7) we easily obtain

$$\varphi \left( \epsilon_{2} \right) = X_{x2} - \frac{4}{3\rho_{0}} \frac{X_{y2}^{2}}{V_{y0}^{2}} E_{2}, \qquad Q \left( \Gamma_{2} \right) = \frac{1}{3\rho_{0}} \frac{X_{y2}^{2}}{V_{y0}^{2}}, \qquad \Gamma_{2} = \sqrt{\epsilon_{2}^{2} + \frac{3}{4} \epsilon_{xy2}^{2}}$$

$$\epsilon_{xy2} = \frac{\rho_{0}V_{y0}^{2}}{X_{y2}}, \qquad \epsilon_{2} = \frac{\rho_{0}V_{y0}^{2} \left( X_{x2} - X_{x0} + \rho_{0}DV_{x0} \right) - X_{y2}^{2}V_{x0}^{2} + V_{y0}V_{y2} \left( X_{x2} - X_{x0} \right)}{X_{y2} \left( \rho_{0}DV_{y2} + X_{y2} \right)}$$

$$(3.2)$$

We see from Formulas (3.2) that by measuring the velocity D of the leading shock-wave and the four quantities  $(V_{x0}, V_{y0}, X_{x2}, X_{y2})$ , on the surface



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of the medium we can establish experimentally the functions  $\varphi(\epsilon)$  and  $Q(\Gamma)$ . To do so it is necessary to vary  $V_{xx}$  and  $V_{yx}$ .

Variant

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$$da_0 / d\epsilon < 0, dQ / d\Gamma > 0$$

A centered pure-compression wave propagates through the undisturbed medium; behind this wave there is a zone of constant flow, through which a compression-shear shock-wave travels. Between the shock-wave and the surface there is a zone of constant flow. This case has been studied in [6]. In the *xt*-plane the motion pattern is as shown in Fig.3. The solution may be written

$$\begin{aligned} \boldsymbol{\varepsilon} &= 0, \quad \boldsymbol{\varepsilon}_{xy} = 0, \quad V_x = 0, \quad V_y = 0 \quad \text{for } x \ge \sqrt{a_0(0)} \ t \\ x / t &= \sqrt{a_0(\varepsilon)}, \quad V_x = -J_1(\varepsilon), \quad \boldsymbol{\varepsilon}_{xy} = 0, \quad V_y = 0, \quad \text{for } \sqrt{a_0(0)} \ t \ge x \ge mt \\ \boldsymbol{\varepsilon} &= \boldsymbol{\varepsilon}_1, \quad V_x = V_{x1}, \quad \boldsymbol{\varepsilon}_{xy} = 0, \quad V_y = 0 \quad \text{for } mt \ge x > Ct \quad (3.3) \\ \boldsymbol{\varepsilon} &= \boldsymbol{\varepsilon}_2, \quad V_x = V_{x0}, \quad \boldsymbol{\varepsilon}_{xy} = \boldsymbol{\varepsilon}_{xy2}, \quad V_y = V_{y0} \quad \text{for } Ct > x \ge 0 \end{aligned}$$

Here

$$J_1(\varepsilon,0) = \int_0 \sqrt[4]{a_0(\varepsilon)} d\varepsilon$$
(3.4)

In order to determine the constants  $e_1$ ,  $e_2$ ,  $e_{xy2}$ ,  $V_{x1}$ , m and C we have the system of equations (2.5) to (2.7), to which we must add

$$m = \sqrt{a_0(e_1)}, \qquad V_{x1} = -J_1(e_1), \qquad X_{x1} = \varphi(e_1) + 4Q(|e_1|)e_1$$
  
Variant 3  
$$da_0 / d|e| > 0, \quad dQ / d\Gamma < 0$$

A pure-compression shock-wave propagates through the undisturbed medium, followed by a zone of constant flow. Then follows a centered shear wave; between this wave and the surface there is constant flow (Fig. 4). An exact solution cannot be written since the equations of a centered shear-wave (2.10) and (2.1) cannot be integrated. One approximate solution can easily be written if the impulse on the surface of the medium is approximately vertical, i.e. if

$$|V_{u0} / V_{x0}| \ll 1$$
 (3.4)

Making the assumption that the order of  $\varphi'$  is higher than (or equal to) that of Q, and estimating the order of the terms in the equations of the shear-wave, we obtain the following approximate solution to the problem

$$\begin{aligned} \varepsilon &= 0, \quad \varepsilon_{xy} = 0, \quad V_x = 0, \quad V_y = 0 \quad \text{for } x > Dt \end{aligned} \tag{3.5} \\ \varepsilon &= \varepsilon, \quad \varepsilon_{xy} = 0, \quad V_x = V_{x1}, \quad V_y = 0 \quad \text{for } Dt > x \geqslant lt \\ x / t = \sqrt{C_0(|\varepsilon|)}, \quad V_x = -J_2(\varepsilon, \varepsilon_1), \quad \varepsilon_{xy} = -\sqrt{2J_3(\varepsilon, \varepsilon_1)} \\ V_y &= J_4(\varepsilon, \varepsilon_1) \quad \text{for } lt \geqslant x \geqslant kt \\ \varepsilon &= \varepsilon_2, \quad \varepsilon_{xy} = \varepsilon_{xy2}, \quad V_x = V_{x0}, \quad V_y = V_{y0} \quad \text{for } kt \geqslant x \geqslant 0 \\ J_2(\varepsilon, \varepsilon_1) &= \int_{\varepsilon_1}^{\varepsilon} \sqrt{C_0(|\delta|)} d\varepsilon + V_{x1}, \qquad C_0(|\varepsilon|) = \frac{3Q(|\varepsilon|)}{\rho_0} \equiv C \bigg|_{\varepsilon_{xy} = 0} \end{aligned}$$

$$J_{3}(\varepsilon, \varepsilon_{1}) = \int_{\varepsilon_{1}}^{\varepsilon} \frac{d\varphi / d\varepsilon + Q(|\varepsilon|) + 4|\varepsilon| Q'(|\varepsilon|)}{Q'(|\varepsilon|)} d\varepsilon$$
(3.6)  
$$J_{4}(\varepsilon, \varepsilon_{1}) = \int_{\varepsilon_{1}}^{\varepsilon} \frac{\sqrt{C_{0}(|\varepsilon|)}}{Q'(|\varepsilon|) \sqrt{2J_{3}(\varepsilon, \varepsilon_{1})}} \left(\frac{d\varphi}{d\varepsilon} + Q(|\varepsilon|) + 4|\varepsilon| Q'(|\varepsilon|)\right) d\varepsilon$$
(3.6)

The constants  $e_1$ ,  $e_2$ ,  $e_{xy2}$ ,  $V_{x1}$ , D, l and k can be found from Equations (2.4), to which must be added the relations

$$l = C_0 V(|\epsilon_1|), \quad k = V \overline{C_0(|\epsilon_2|)}, \quad -J_2(\epsilon_2, \epsilon_1) = V_{x0}, \quad J_4(\epsilon_2, \epsilon_1) = V_{y0}$$

$$\epsilon_{xy2} = -V \overline{2J_3(\epsilon_2, \epsilon_1)} \quad (3.7)$$

$$da_0 / d|\epsilon| < 0, \quad dQ / d\Gamma < 0$$

A centered pure-compression wave propagates through the undisturbed medium, followed by a zone of constant flow. Then follows a centered shear-wave between which and the surface there is a zone of constant flow (Fig.5). The solution, when conditions (3.4) are satisfied, is of the form

$$\mathbf{\varepsilon} = 0, \quad \mathbf{\varepsilon}_{xy} = 0, \quad V_x = 0, \quad V_y = 0 \quad \text{for } x \ge \sqrt{a_0(0)} \ t \qquad (3.8)$$

$$x \ / \ t = \sqrt{a_0(\mathbf{\varepsilon})}, \quad V_x = -J_1(\mathbf{\varepsilon}), \quad \mathbf{\varepsilon}_{xy} = 0, \quad V_y = 0 \quad \text{for } \sqrt{a_0(0)} \ t \ge x \ge mt$$

$$\mathbf{\varepsilon} = \varepsilon_1, \quad V_x = V_{x1}, \quad \mathbf{\varepsilon}_{xy} = 0, \quad V_y = 0 \quad \text{for } mt \ge x \ge lt$$

$$x \ / \ t = \sqrt{C_0(|\mathbf{\varepsilon}|)}, \quad V_x = -J_2(\mathbf{\varepsilon}, \mathbf{\varepsilon}_1), \quad V_y = J_4(\mathbf{\varepsilon}, \mathbf{\varepsilon}_1)$$

$$\mathbf{\varepsilon}_{xy} = -\sqrt{2J_3(\mathbf{\varepsilon}, \mathbf{\varepsilon}_1)} \quad \text{for } lt \ge x \ge kt$$

$$\boldsymbol{\varepsilon} = \boldsymbol{\varepsilon}_2, \quad \boldsymbol{\varepsilon}_{xy} = \boldsymbol{\varepsilon}_{xy2}, \quad V_x = V_{x0}, \quad V_y = V_{y0} \quad \text{for } kl \ge x \ge 0$$

The constants  $e_1, e_2, e_{xy2}, V_{x1}, m, l$  and k can be found from Equations (3.6), together with the relations

$$m = \sqrt{a_0(\varepsilon_1)}, \quad V_{x1} = -J_1(\varepsilon_1) \quad (3.9)$$

4. We consider now the experimental determination of the functions  $\omega(\varepsilon)$  and  $Q(\Gamma)$ . As has already been pointed out, it is possible that a medium exists for which in the case of small deformations  $da_0/d|\varepsilon| > 0$ ,  $dQ/d\Gamma > 0$ . For such a medium formulas (3.2) can be used to derive experimental relations  $\varphi(\varepsilon)$  and  $Q(\Gamma)$  by subjecting a medium (for example, soil) to an oblique impact at the surface. However, although the limitation  $da_0/d|\varepsilon| > 0$  will be satisfied (for instance, in expariments of pure compression a shock-wave is fixed in a soil [3 and 4]), the assumption



Fig. 5

In a soil [3 and 4]), the assumption that  $dQ/d\Gamma > 0$  is open to dispute. So far no experiments have been carried out on materials, in particular in soils, in shear-compression; therefore the question of whether the shear-compression wave is a shock-wave  $(Q' \ge 0)$  or whether it is continuous (Q' < 0) remains unanswered experimentally. Experimental curves drawn from Formulas (3.2) must therefore be verified. This can be done by an experiment in pure compression  $(V, \equiv 0)$ .

The solution for  $da_o/d|\epsilon| > 0$  (a shock-wave in front followed by constant flow) in the case of pure compression is of the form

$$\boldsymbol{\varepsilon} = 0, \quad V_x = 0, \quad X_x \doteq X_{x0} \quad \text{for } x > Dt$$
 (4.4)

$$\boldsymbol{\varepsilon} = \boldsymbol{\varepsilon}_1, \quad V_{\boldsymbol{x}} = V_{x0}; \quad X_x = X_{y1} \quad \text{for } Dt > x \ge 0$$

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If  $V_x$  is given, then  $\epsilon_1$  and D (the velocity of the shock-wave) can be found from Equations (2.4) in which we set  $V_{x1} = V_{x0}$ . Remembering that in this case  $Y_y = Z_x$  and therefore  $\phi = \frac{1}{3}(X_x + 2Y_y)$ , we conclude that experimental curves for  $\phi(\epsilon)$  and  $Q(\Gamma)$  can be drawn if in an experiment of pure compression  $(V_y \equiv 0)$  we measure  $V_{x0}$ , D and  $Y_{y1}$  ( $Y_{y1}$  is the value of  $Y_y$  at the surface of the soil). The solution of the problem is

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$$\varepsilon_{1} = -\frac{V_{x0}}{D}, \quad \varphi(\varepsilon_{1}) = \frac{1}{3} \left( X_{x0} + 2Y_{y1} - \rho_{0} DV_{x0} \right)$$
$$Q(|\varepsilon_{1}|) = \frac{1}{6} \frac{\rho_{0} DV_{x0} - X_{x0} + Y_{y1}}{V_{x0}} D$$
(4.2)

A second check on the accuracy of the results obtained is provided by a comparison of the relations  $\varphi(\varepsilon)$ , obtained in the manner indicated from Formulas (3.2), with those obtained by the well-known experiment on hydrostatic compression described in [5].

If the function  $Q(\Gamma)$  obtained from Formulas (4.2) is found to decay (Q' < 0), then the solution (3.1) and Formulas (3.2) are not applicable to the calculation of a shear-compression impact. A check on the validity of experimental curves for  $\varphi(\varepsilon)$  and  $Q(\Gamma)$  obtained from (4.2) is provided in this case by the solution to the problem of shear-compression impact given by the formulas of variant 3 with experimentally determined parameters (for example, the velocity D of the shock-wave, the stresses  $X_1$ ,  $X_2$  at the surface of the soil). The solution to the problem is then given on the basis of experimental functions  $\varphi(\varepsilon)$  and  $Q(\Gamma)$ .

## BIBLIOGRAPHY

- Loitsianskii, L.G., Mekhanika zhidkosti i gaza (Liquid and Gas Mechanics). Gostekhizdat, 1957.
- Landau, L.D. and Lifshits, E.M., Mekhanika sploshnykh sred (Mechanics of Continuous Media). Gostekhizdat, 1953.
- Grimza, Iu.M., Priamoi eksperimental'nyi metod postroeniia udarnykh diagramm szhatila gruntov (A direct experimental method of deriving impact curves in the compression of soils). Primenenie vibratsii v stroitel'stve, Sb. № 51, 1962.
- 4. Grimza, Iu.I., Nekotorye rezul'taty eksperimental'nykh issledovanii po opredeleniiu skorosti rasprostraneniia prodol'nykh voln v obraztsakh grunta (Some results of experimental investigations into the determination of the velocity of propagation of longitudinal waves in soil specimens). Dinamika gruntov, Sb. № 44, M., 1944.
- Grigorian, S.S., Ob osnovnykh predstavleniiakh dinamiki gruntov (On basic concepts of soil dynamics). PMM Vol.24, № 6, 1960.
- Rakhmatulin, Kh.A., O rasprostranenii volny slozhnogo nagruzheniia (On the propagation of a wave of combined loading). PMN Vol.22, № 6,1958.
- Zhubaev, N., O rasprostranenii udarnykh voln nagruzki i nagruzka razgruzka v deformatsionnoi modeli grunta (On the propagation of loading waves and loading - unloading in a deformable soil model). Vestn.Akad. Nauk Kazakh.SSR, № 9, 1963.
- Zhubaev, N. Issledovanie rasprostraneniia udarnykh voln v gruntakh (An investigation of the propagation of shock-waves in soils). Vestn.Akad. Nauk Kazakh.SSR, № 3, 1964.